

# Coker Heaters Performance Improvement

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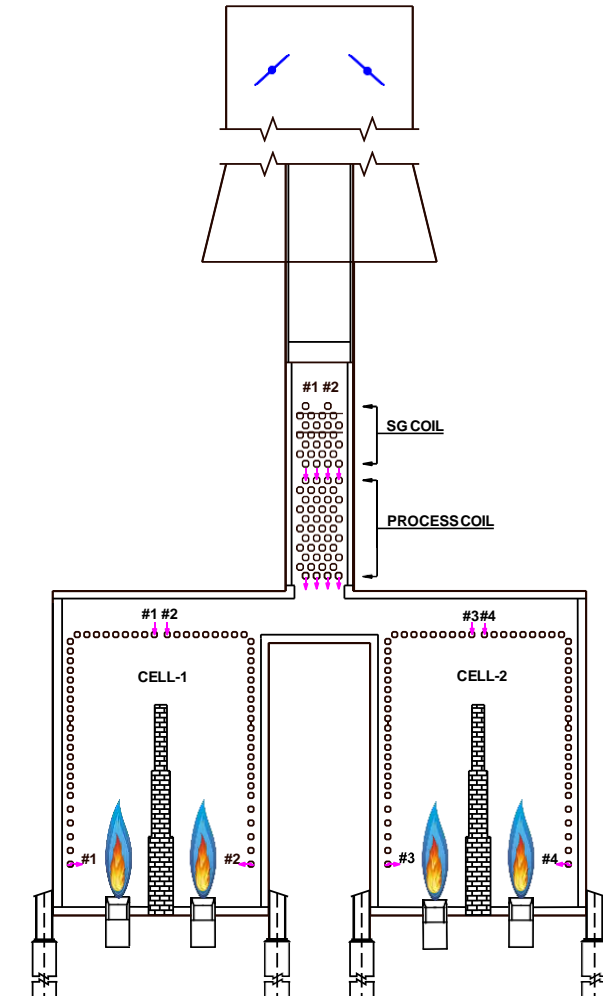


# Coker Heaters

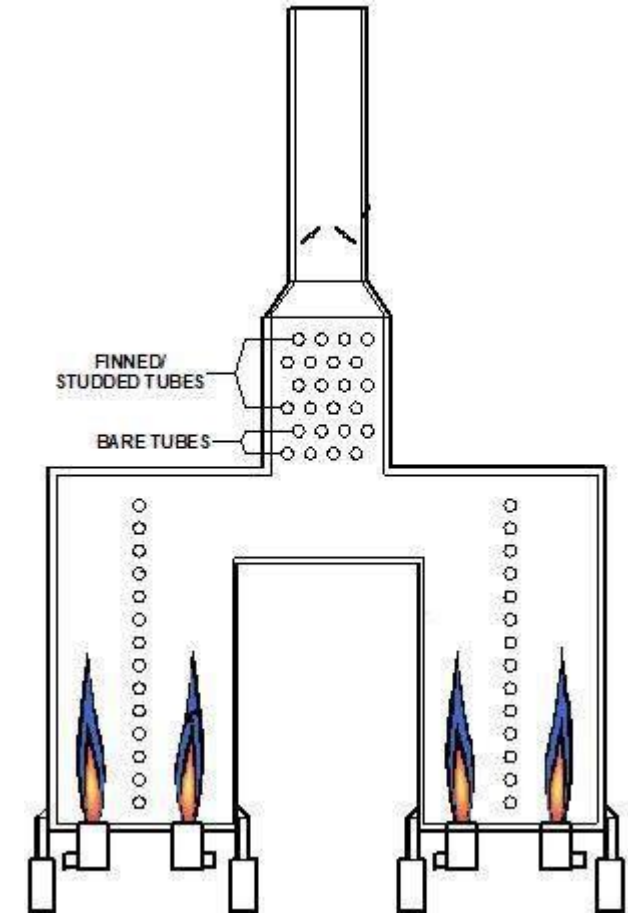
- Most critical heaters in the refineries
- Heart of Delayed Coker Unit (DCU)
- Objective: Process asphalt-like material to higher value products, such as gasoline, diesel fuel, LPG, and petroleum coke
- Charge is rapidly heated to the desired temperature
- Delayed coking is an endothermic reaction with the heater supplying the heat
- Coking in Tubes:
  - Pressure drop goes up
  - High tube metal temperature
- Steam is injected to minimize the cracking until it is in the Coke Drum.
- The rate of coke deposition determine Coker heater run length.

# Coker Heater Types

- Horizontal tube cabin heaters
- Single or double fired
- Advantages of double-fired Coker heater over single fired heater
  - Shorter coil
  - Higher heat flux
  - Lower pressure drop
  - Lower residence time
  - More uniform heating of metals



**Single Fired**



**Double Fired**

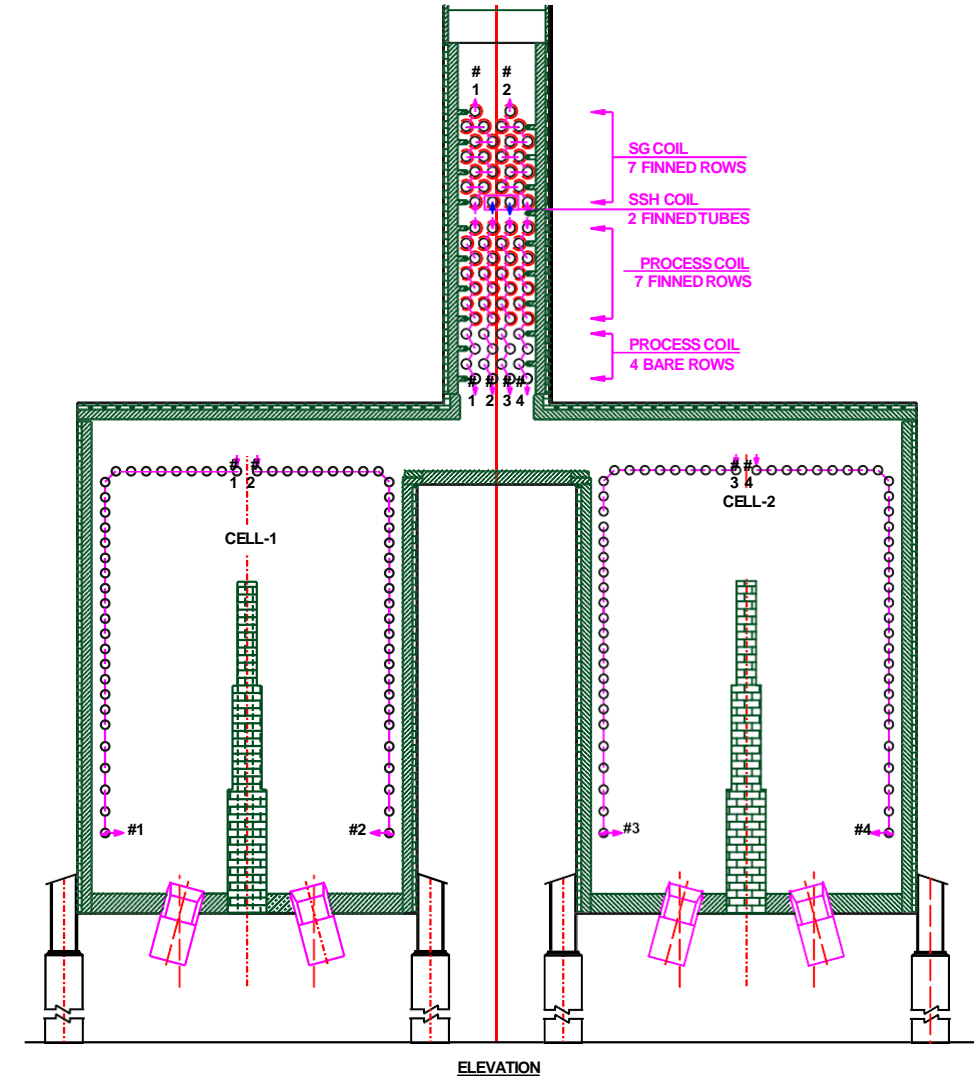
# Coker Heater Design Parameters

- Inlet temperature
  - 400-600°F
- Outlet temperature
  - 900-950°F
- Coil Pressure Drop
  - 350-450 Psi (EOR)
- Condensate/Steam Flow Rate
  - 0.5-1 % of heater feed but highly dependent on the flow rate to each pass
- Average Heat Flux
  - < 9,000 Btu/hr ft<sup>2</sup> (Single Fired)
  - 12,500 – 13,000 Btu/hr ft<sup>2</sup> (Double Fired)
- ❖ Mass velocity-
  - 350-550 lbs/sec ft<sup>2</sup>
- ❖ Cold oil velocity
  - around 6-10 ft/s



# Lyondell 736 Coker Heater Case Study

Parameters	Units	Value
Total Heat Duty	MMBtu/hr	125.10
Process Heat Duty	MMBtu/hr	112.0
Charge Rate	BPD	17,000
Inlet / Outlet Temperature	°F	550 / 950
Inlet / Outlet Pressure	psig	410 / 60
Condensate Flow Rate	lb/hr	1,167
Firing Rate	MMBtu/hr	144



**Existing Coker Heater**

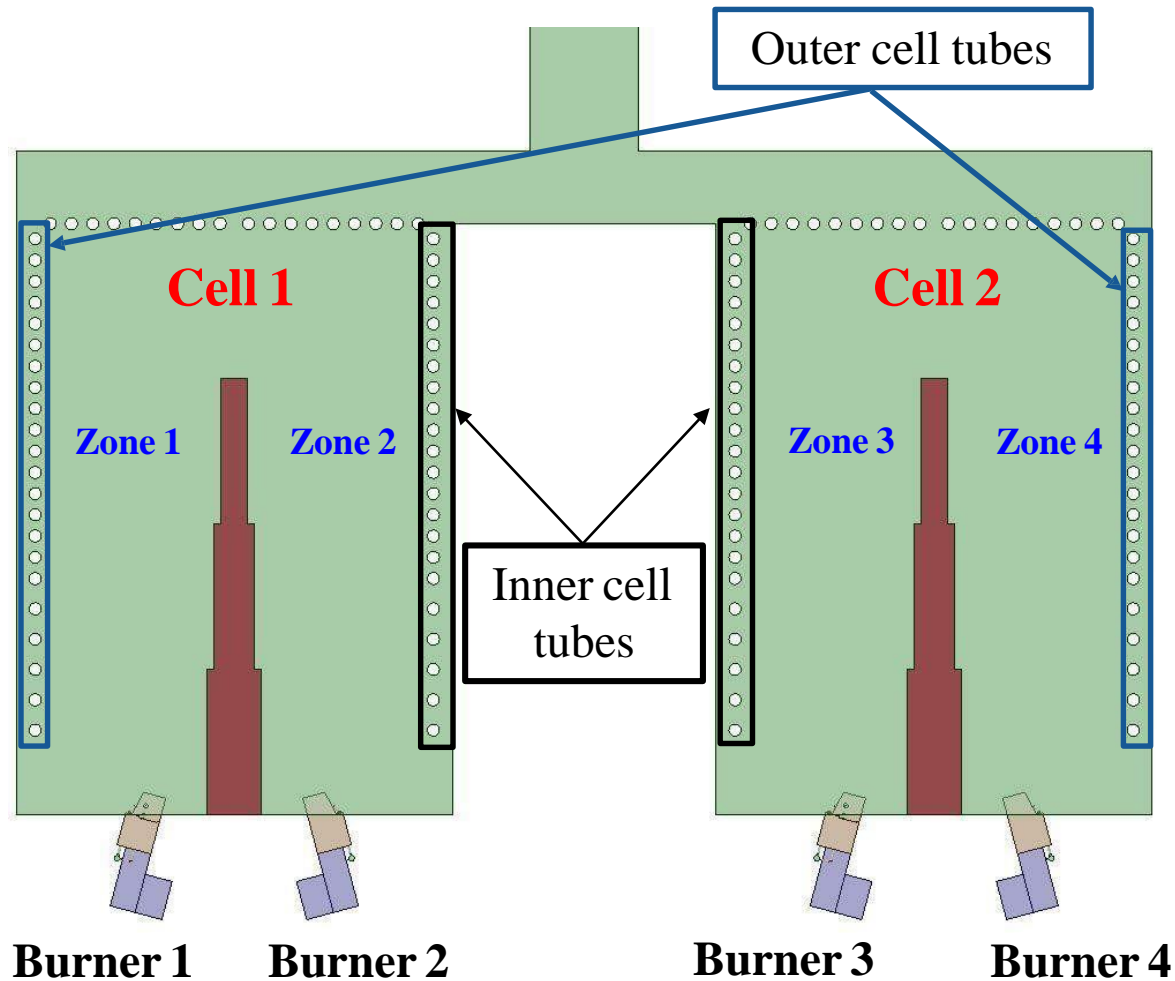
# Lyondell 736 Coker Heater Issues

- Coking
  - Frequent decoking requirement (every year)
  - Short tube life around 5.7 years only- Increase to 14 years
- ❖ Overheating and flame impingement on roof tubes
  - Longer flame lengths
  - Low roof tubes elevation
  - Tube failures
- ❖ Stack
  - Draft at arch -0.3” WC to -0.5” WC
  - Poor flame patterns
- ❖ Tramp Air
  - Leakage of tramp air into the heater due to higher draft operation

# Existing Heater Design Observation

- Flue gas temperature leaving radiant section –1,620°F
- The flue gas mass velocity in convection section is 0.5 lb./sec.ft<sup>2</sup>
- The flue gas convection exit temperature is 800°F from process coil
- There are 48 burners arranged in 4 rows in both cells.
- Coker heaters are designed for a higher average radiant heat flux of 10,000 Btu/hr.ft<sup>2</sup>.
- Calculated charge mass velocity is only 295 lbs./sec.ft<sup>2</sup> (SOR case)
  - This is very low for the Coker heaters.
  - The typical recommended Coker heater mass velocity is in the range of 350-450 lbs./sec.ft<sup>2</sup>.
  - Minimum Cold oil velocity in Coker heaters is 6 ft/sec.
- The draft mentioned at burners is only 0.3 inch WC
- The ultralow NO<sub>x</sub> burners currently installed have very long flames

# Existing Design Geometry for CFD

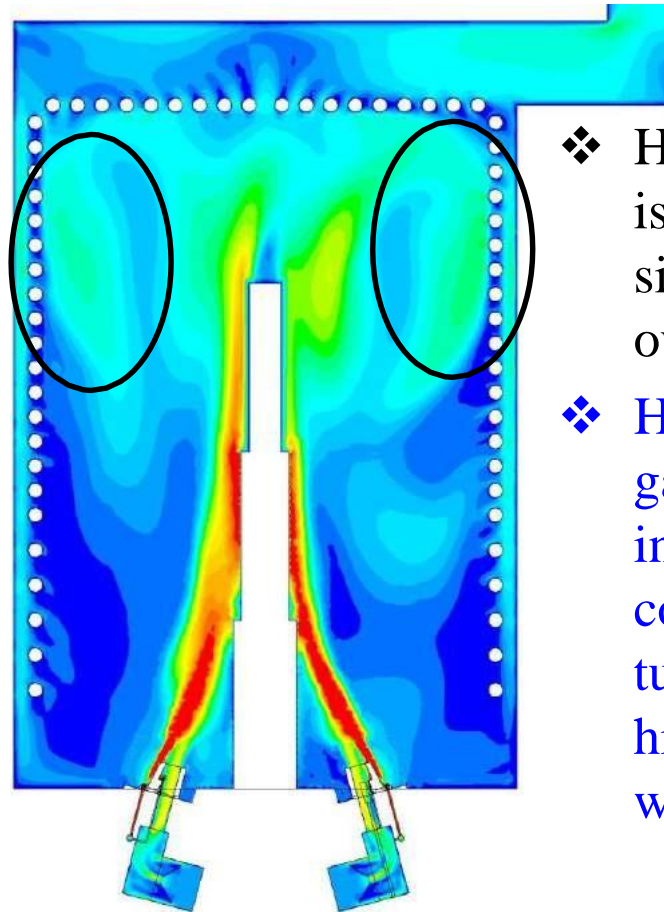
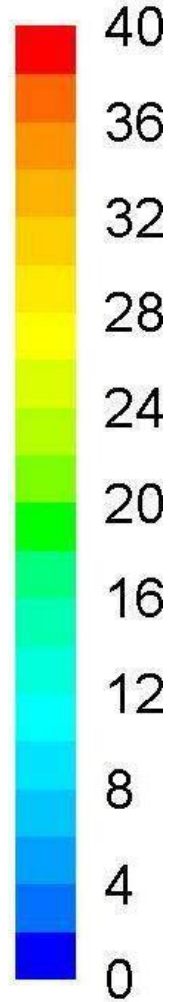


- ❖ No. of burners in CFD model: 4
- ❖ Design heat release per burner: 3.0 MMBtu/hr
  - Fuel flow rate per burner: 154.7 lb/hr
  - Air flow rate per burner: 2,928 lb/hr



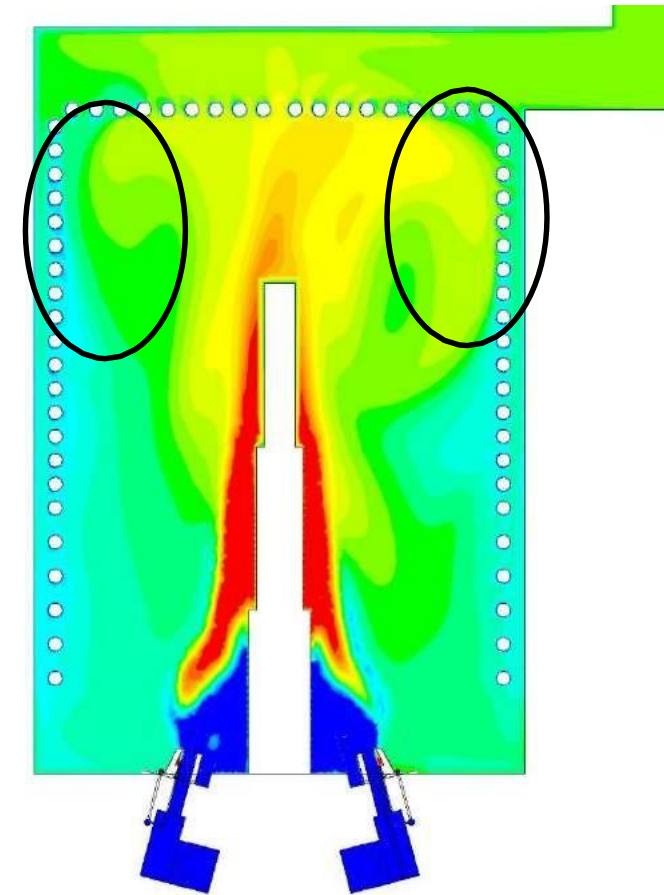
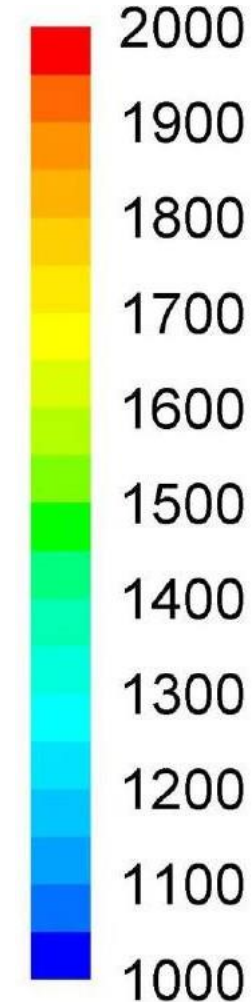
# Flue Gas Flow and Temperature Profile

[ft/s]



- ❖ Higher velocity flue gas is observed on the inner side as compared to the outer side
- ❖ Higher temperature flue gas is observed near the inner cell tubes as compared to the outer cell tubes. This indicates higher heat exchange with the inner cell tubes.

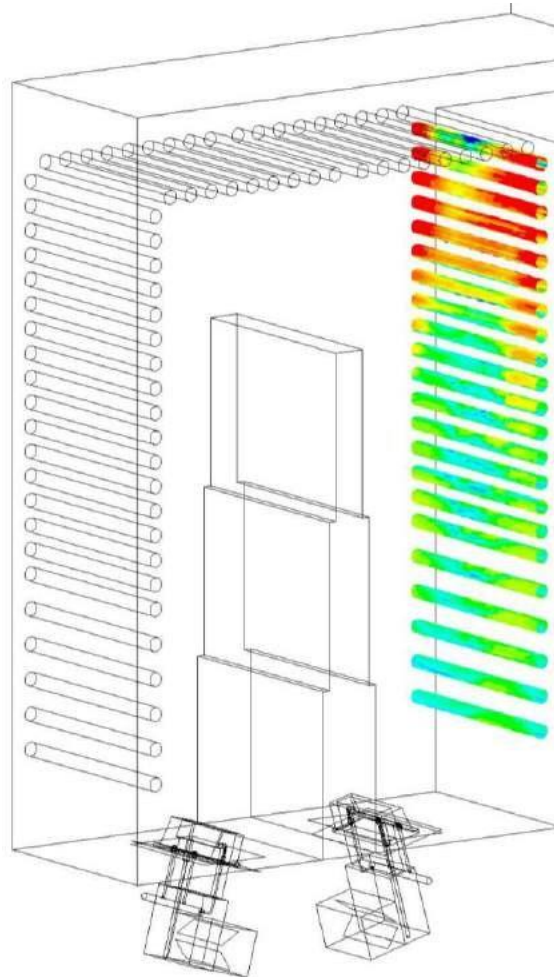
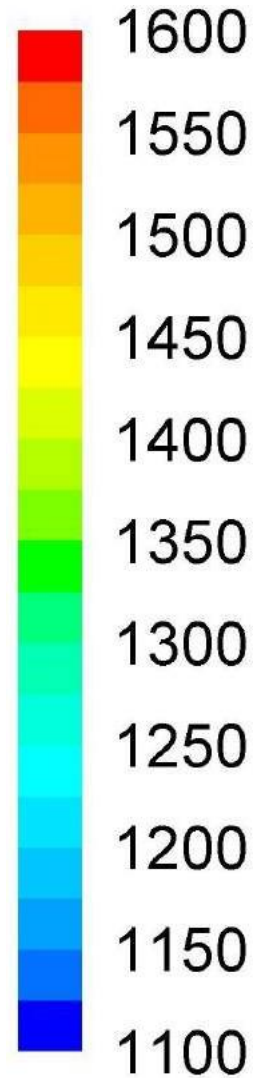
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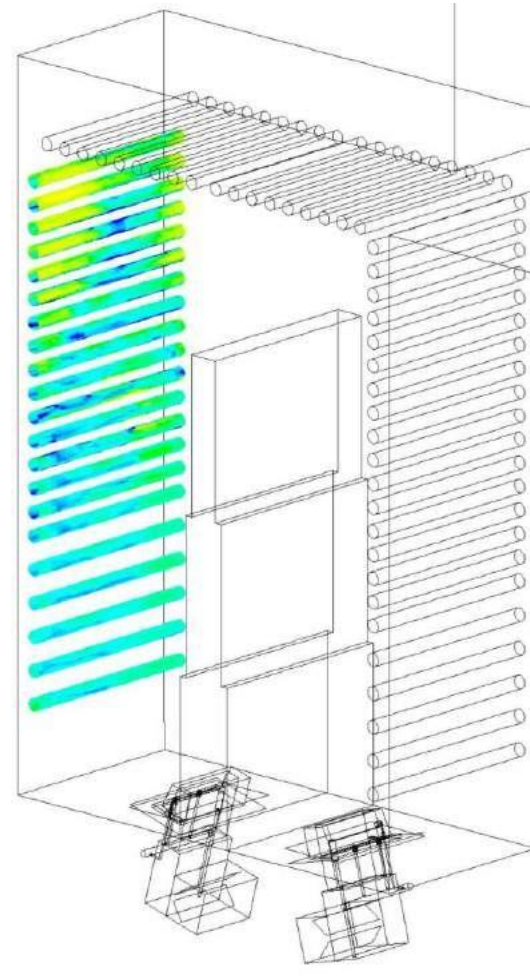
Firing rate for all burners is same: 3 MMBtu/hr

# Flue Gas Temperature around Tubes

[°F]



**Inner Tubes**

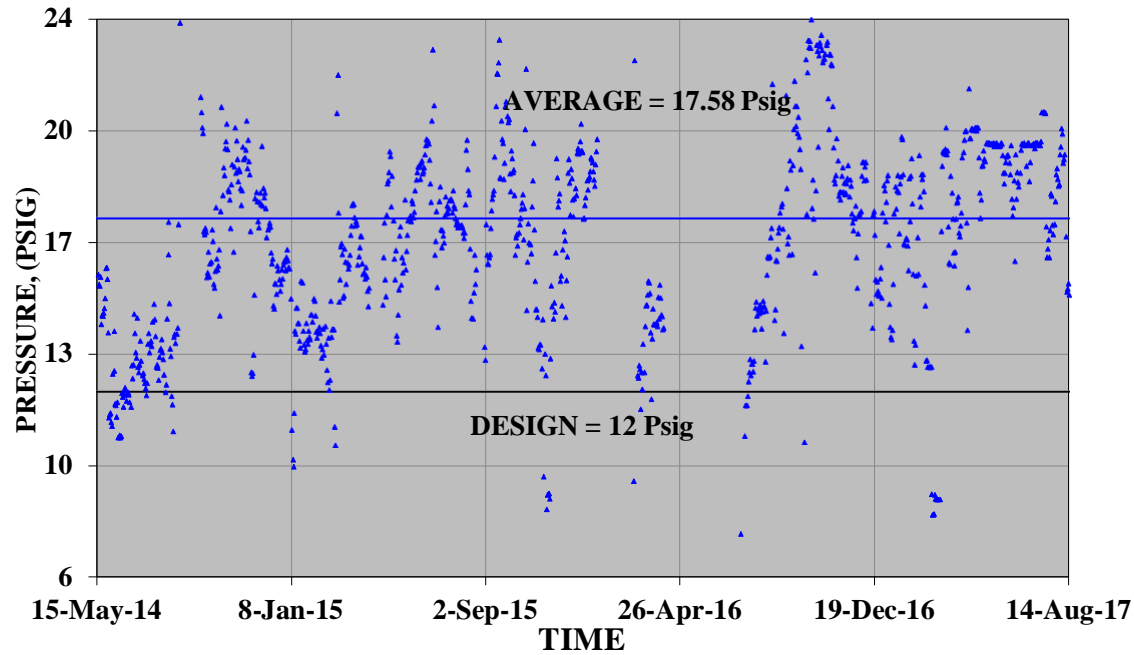


**Outer Tubes**

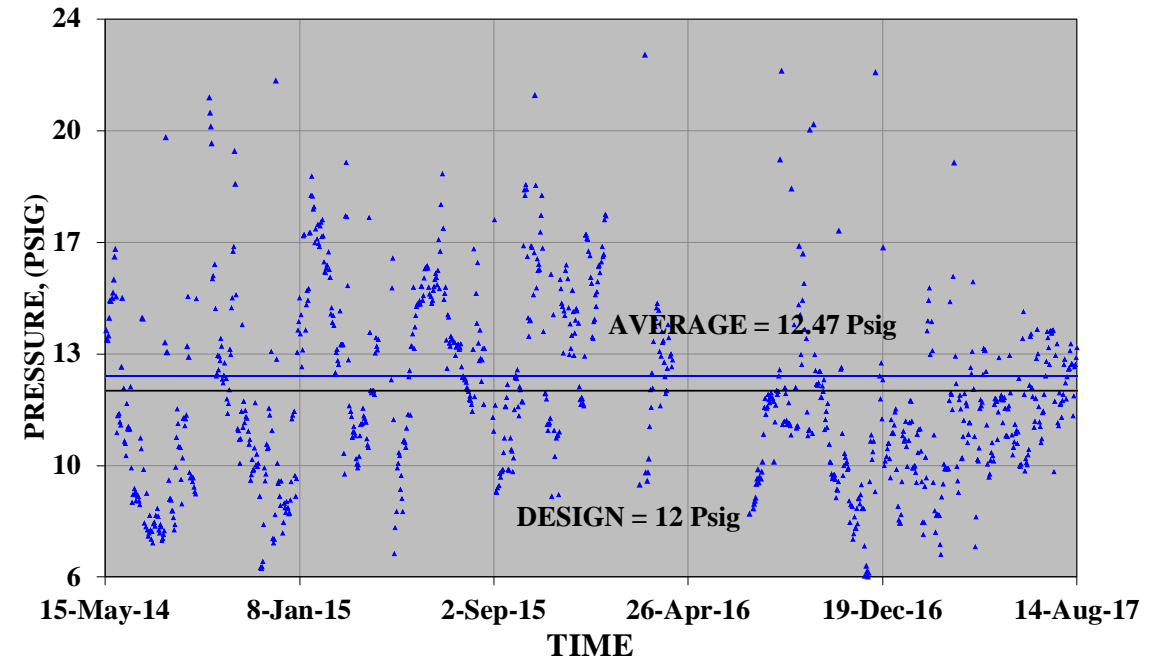
**Existing Design**

- ❖ Flue gas temperatures around inner cell tubes and outer cell tubes are significantly different. This is due to the inclination of flow towards the convection section.

# Fuel Gas Pressure



**West Outer Cell**

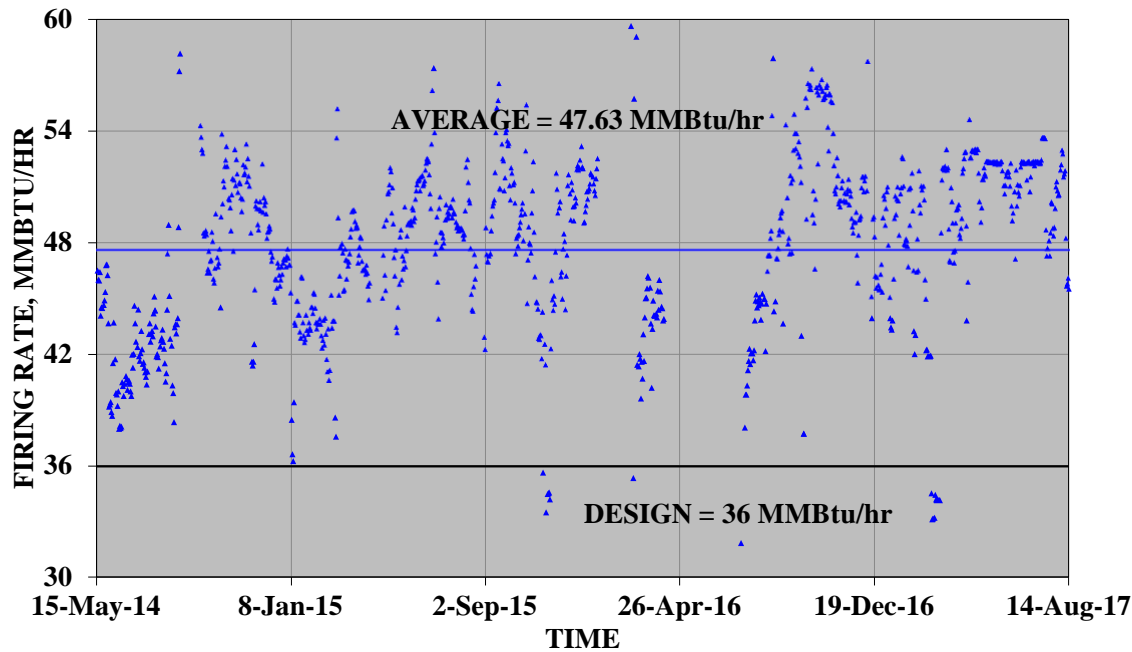


**West Center Cell**

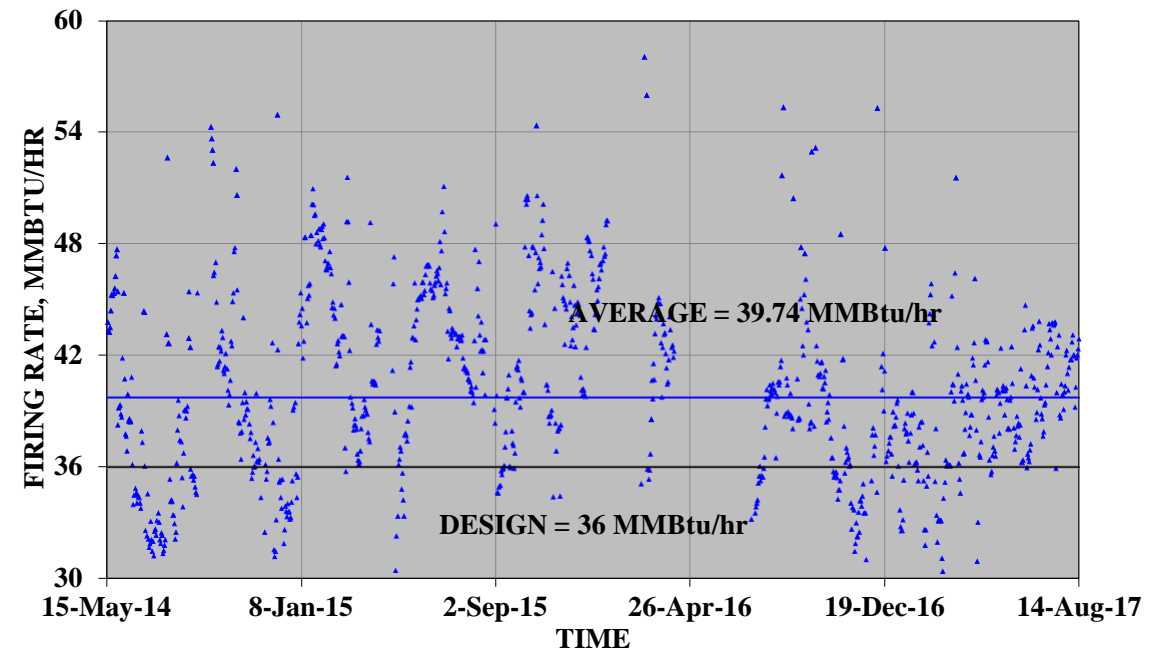
Fuel gas pressure in the outer cell is almost 40% higher than the fuel gas pressure in the inner cells.



# Firing Rate based on Fuel Gas Pressure



**West Outer Cell**



**West Center Cell**

Fuel gas flow in the outer cell is almost 20% higher than the fuel gas flow in inner cell.

# Existing Heater Operating Observation

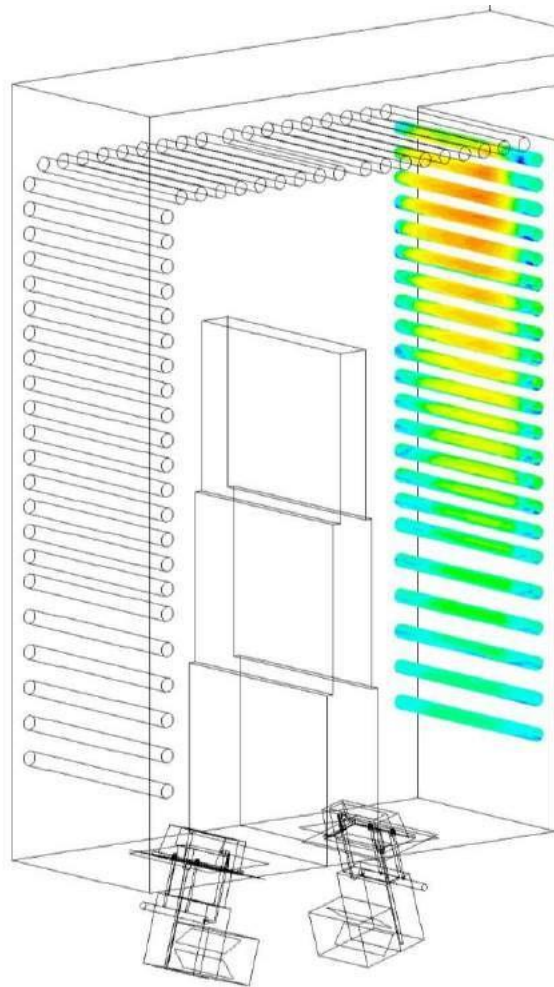
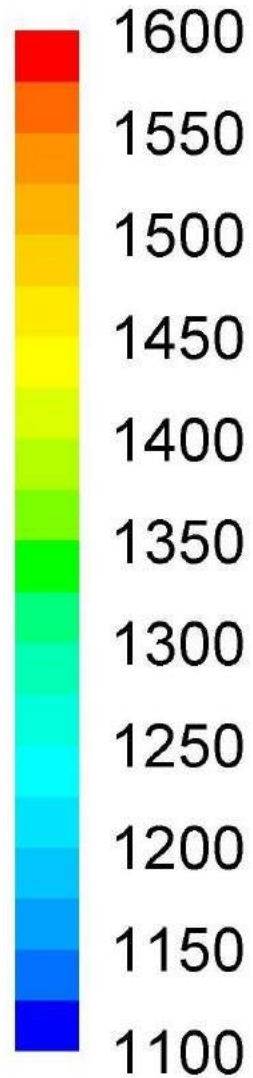
- Current operating pressure drop is 210 psi ( lower by 140 psi)
- Heater outlet temperature is 915°F ( lower by 35 F)
- The flue gas approach temperature to Coker feed is 250-300°F, which is very high
- Total firing rate in the heater is 18% higher than the design firing rate.

Parameters	Units	West Outer Cell	West Center Cell	East center Cell	East Outer Cell
Design Firing Rate	MMBtu/hr	36.0			
Average Firing Rate	MMBtu/hr	47.3	39.2	37.9	45.1
Firing Rate for CFD model	MMBtu/hr	3.0	2.3	2.3	3.0

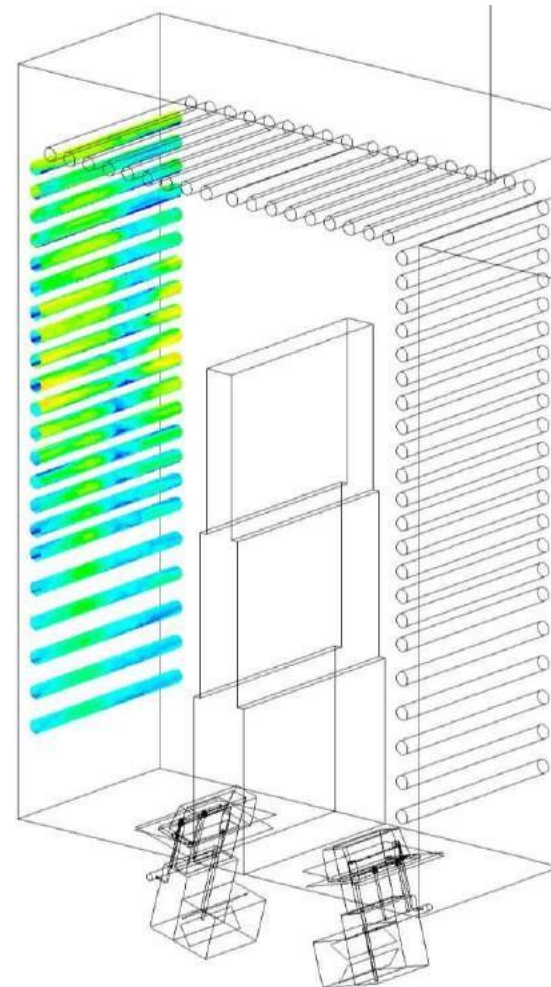


# Flue Gas Temperature around Tubes

[°F]



**Inner Tubes**

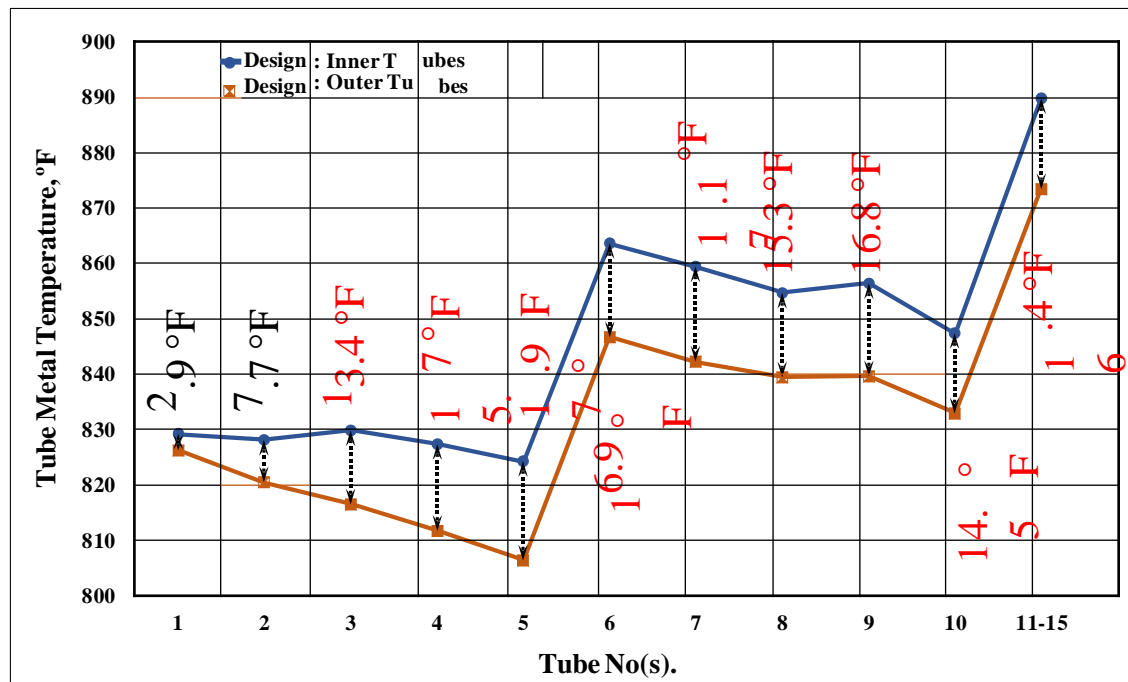


**Outer Tubes**

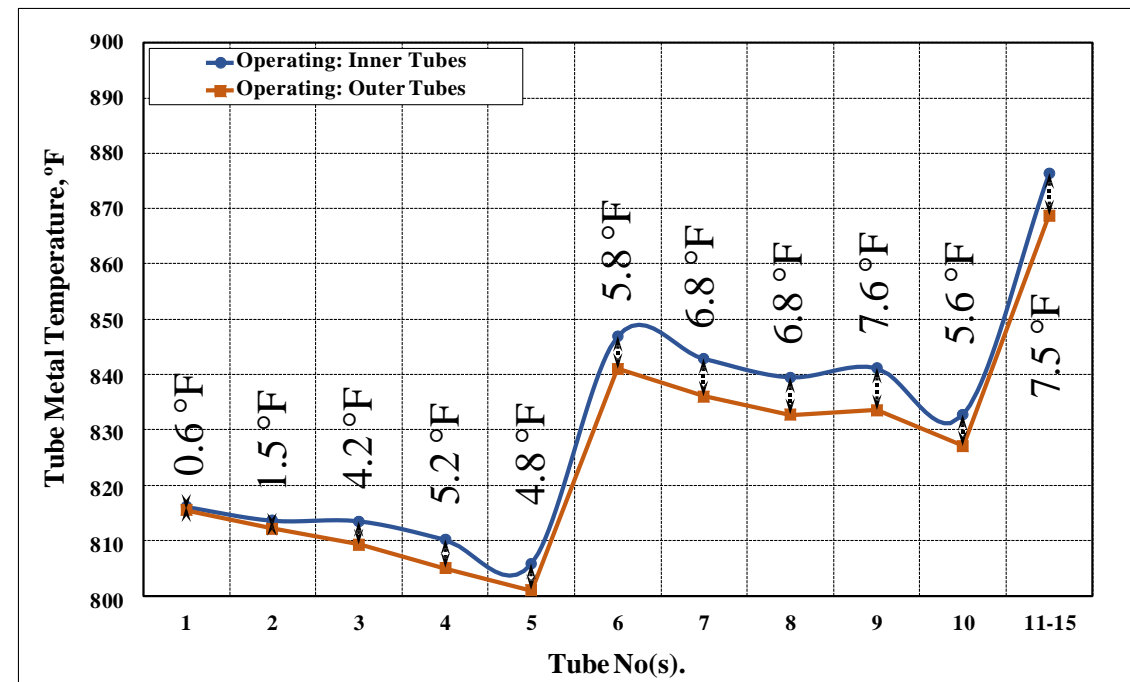
**Existing Operating**

- ❖ Clearly, the difference in flue gas temperatures around inner and outer cell tubes have reduced significantly as compared to the design case
- ❖ Flue gas temperature around inner tubes was reduced by 75 -100 °F

# TMT Comparison with Existing Design



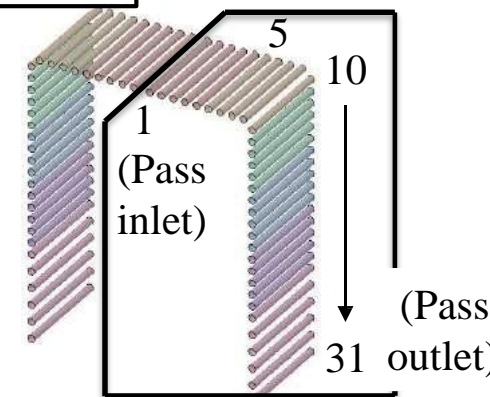
**Existing Design**



**Existing Operating**

TMT difference between the inner and outer tubes has decreased for each of the tubes for the operating case where inner cell burners fire 20% lower than the outer cell burners.

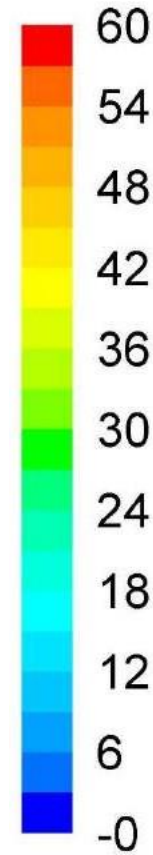
Comparison is done only for roof tubes and few tubes in the top section of the heater



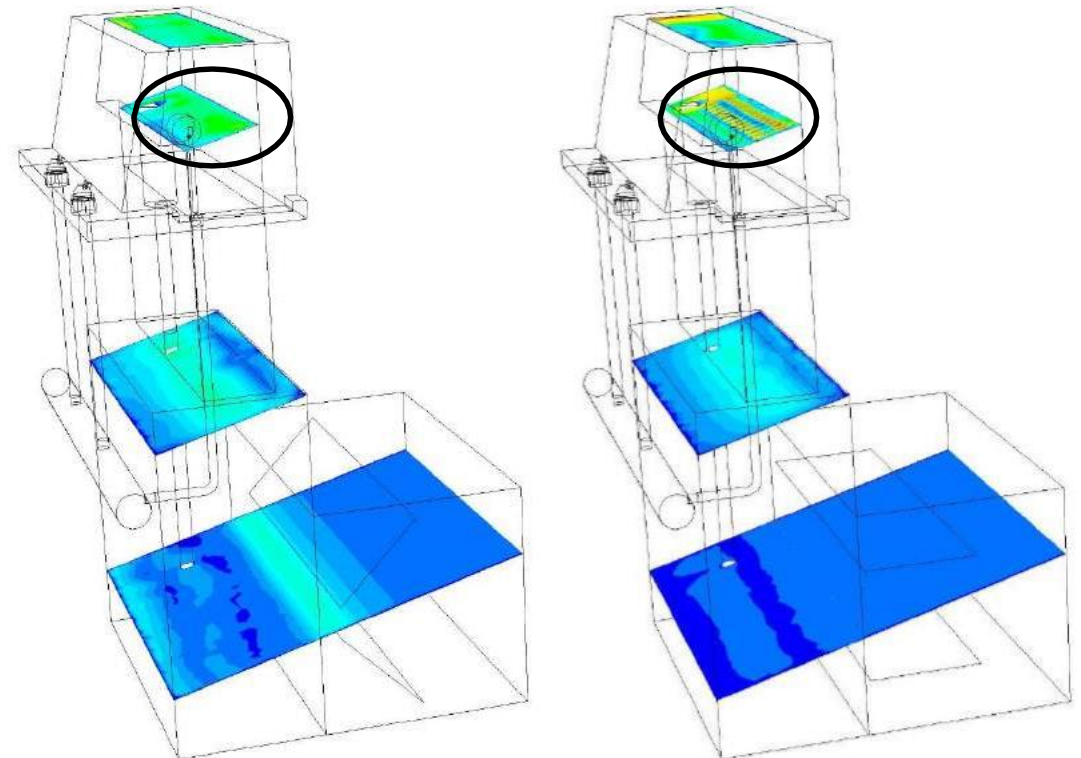
# Burners Modification

- Existing burners were not utilizing the full heater floor draft available as well as full fuel gas pressure available at the tips.
- To improve the flame pattern and heat distribution in the radiant section, a pressure drop plate was installed at the burner throat
- This increases the air side pressure drop, improves the fuel air mixing and gives a better flame pattern

[ft/s]



## Velocity Profile



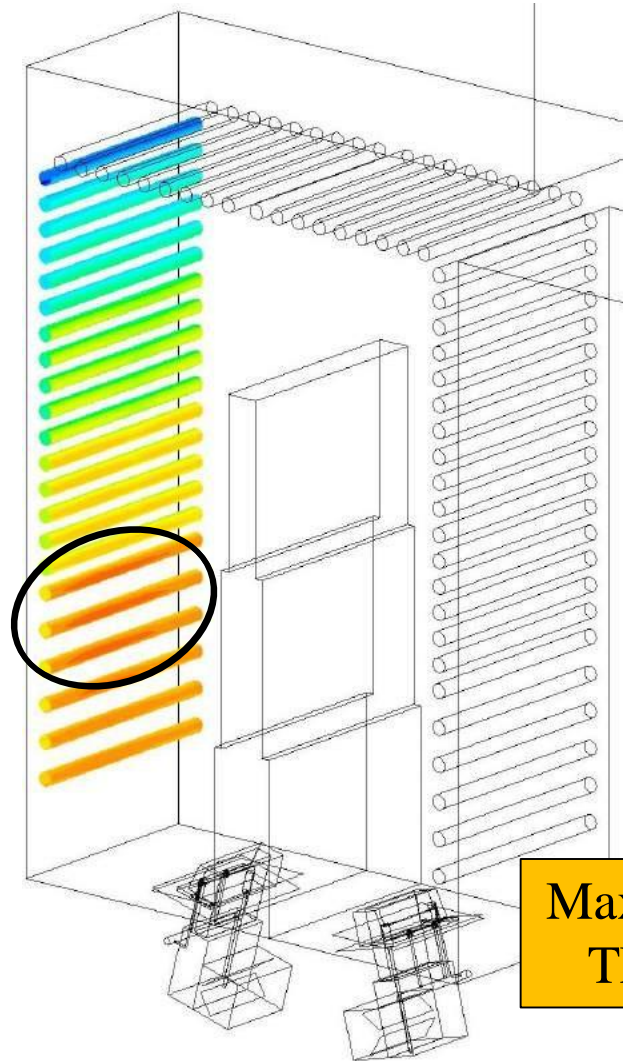
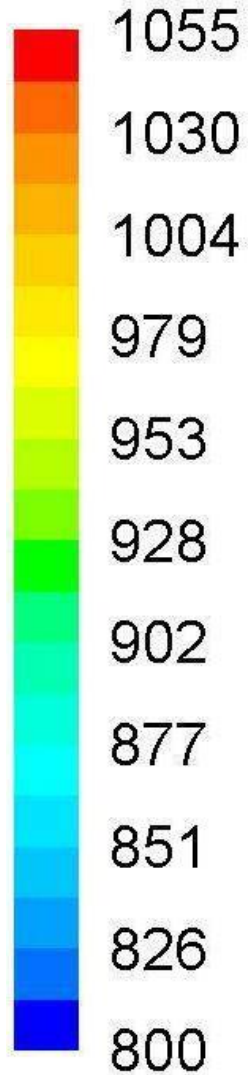
Existing

Proposed



# Radiant TMT profile- Outer Tubes

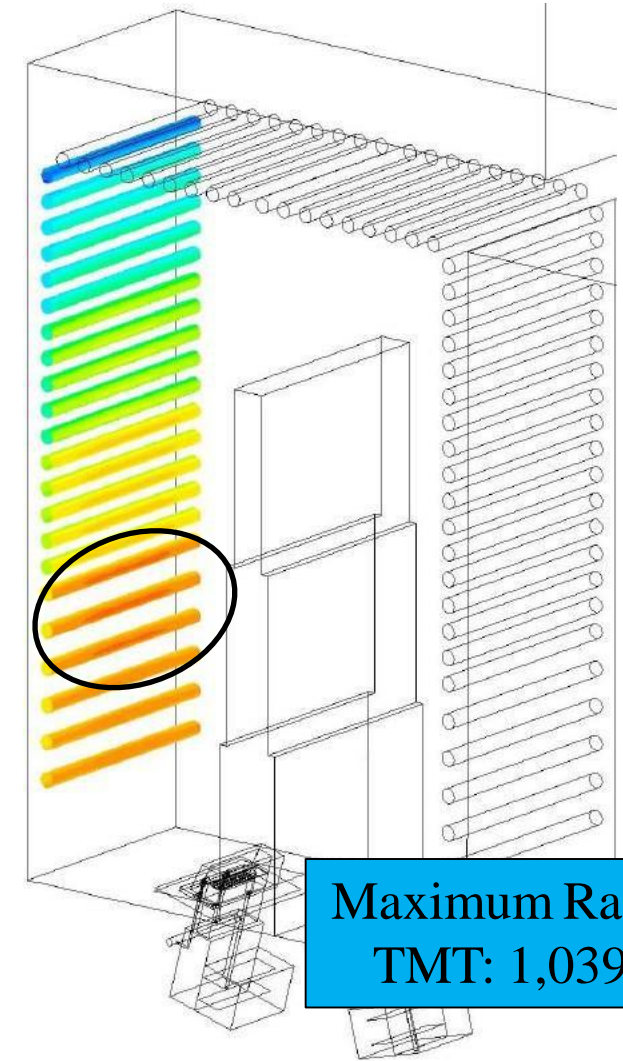
[°F]



**Existing**

Maximum Radiant  
 TMT: 1,044 °F

Reduction in TMT is observed  
 on these radiant tubes with  
 burner modification



**Burner Modification**

Maximum Radiant  
 TMT: 1,039 °F

# Radiant Re-Tubing Proposed Options

	Tube Details	Total No. of Radiant Tubes	Material
Existing	3.5” NPS Sch 80	62	9 Cr-1Mo Material
Proposed Option-1	4” OD, 0.4” MWT	66	9 Cr-1Mo Material
Proposed Option-2			SS347H Material
Proposed Option-3 (Finalized Option)	4.25” OD, 0.5” MWT		9 Cr-1Mo Material

- Upgrading the tube material to SS-347H increases spalling temperature to 1,300°F. SS347H tubes can be operated up to 1,500°F design tube metal temperature
- The arch tubes for all the proposed options are shifted closer to arch refractory.



# Radiant Coil Re-Tubing

## Existing Design

- No. of radiant tubes: 62 per cell
- Tube size: 3.5” NPS Sch 80
- Tube length: 60 ft 9 inches
- Heat transfer area: 7,770 ft<sup>2</sup>
- Tube material: A335 Gr. P9
- Tube are approaching end of life
- Low roof tubes elevation
- High radiant TMT

## Final Proposed Design

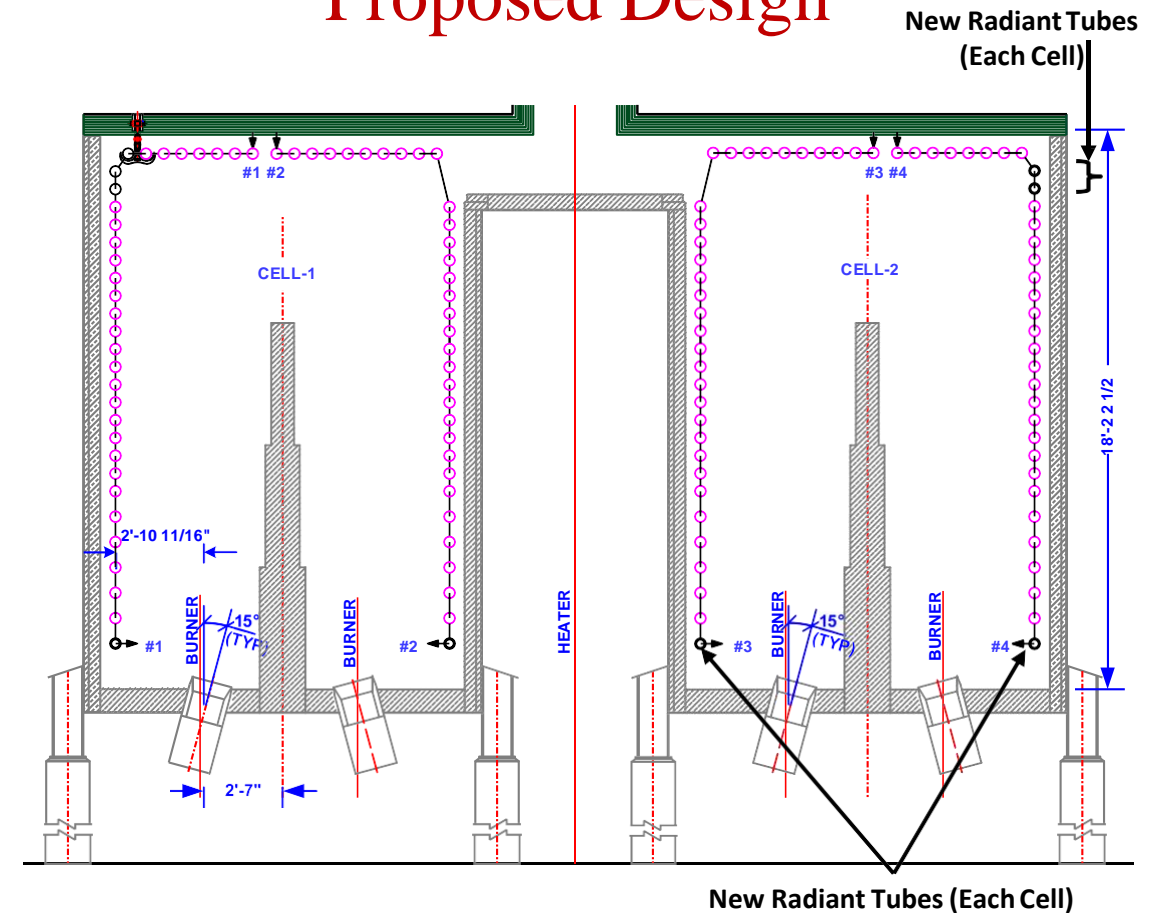
- Total radiant tubes: 66 per cell
  - Addition of 4 new radiant tubes
  - 2 tubes installed at outlet and 2 at roof
- Tube size: 4.25” OD, 0.5” MWT
- Heat transfer area: 8,922 ft<sup>2</sup>
- Tube material: A213 Gr.T9
- Roof tubes will be shifted closer to arch by 16”

Radiant Heat transfer Area increased by 15% in the heater.

# Raising of Roof Tubes

- The ultralow NO<sub>x</sub> burners currently installed have very long flames
- The burner to roof tubes distance barely meets the minimum distance between burner and roof tubes specified by API-560
- The existing radiant tubes at the roof will be shifted up towards the arch, such that the tubes are backed by the refractory to reduce flame impingement on the tubes
- This will move the roof tubes out of the flue gas path to the convection section

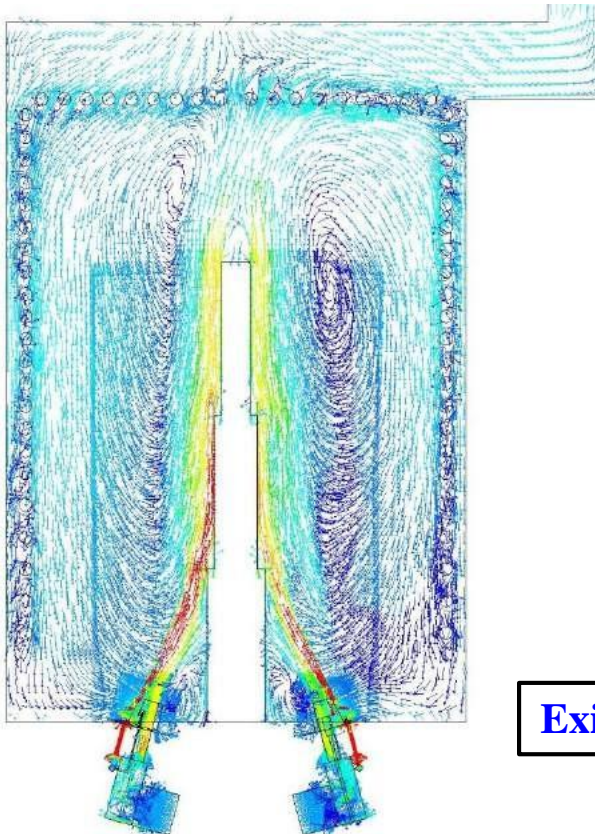
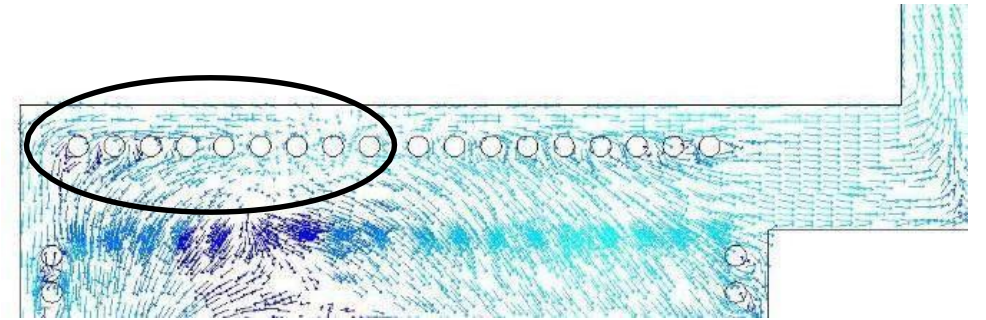
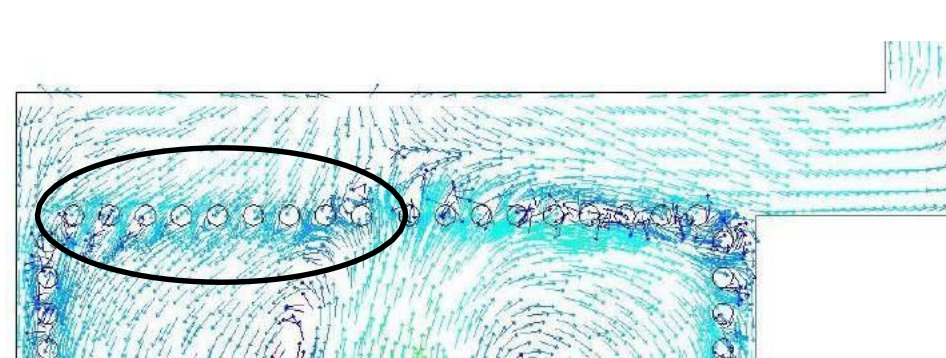
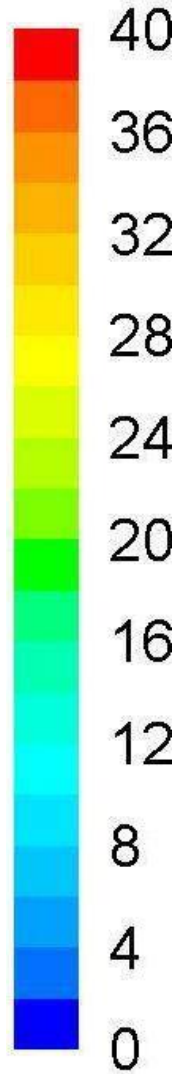
## Proposed Design





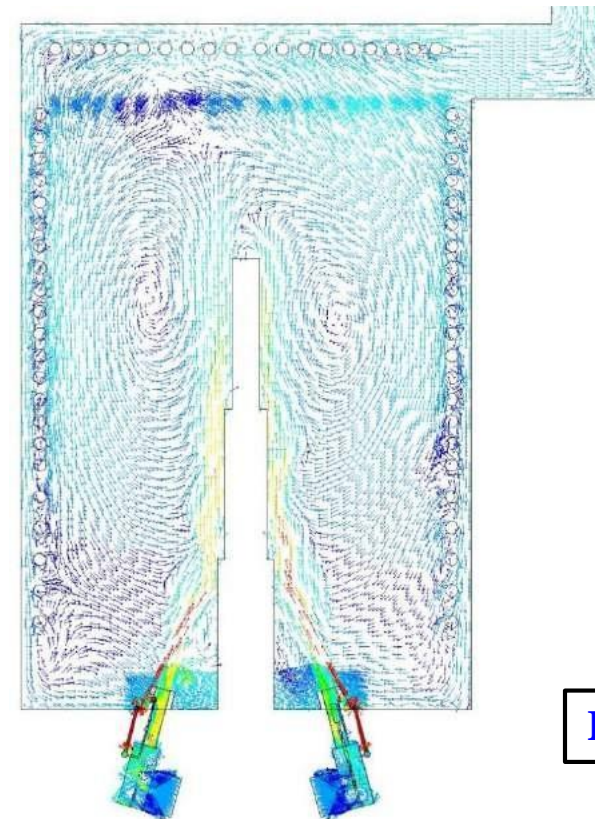
# Flue Gas Velocity Vectors

[ft/s]



Recirculation around roof tubes has reduced for raised tubes case

Longer flue gas recirculation path is observed in the proposed case with raised roof tubes



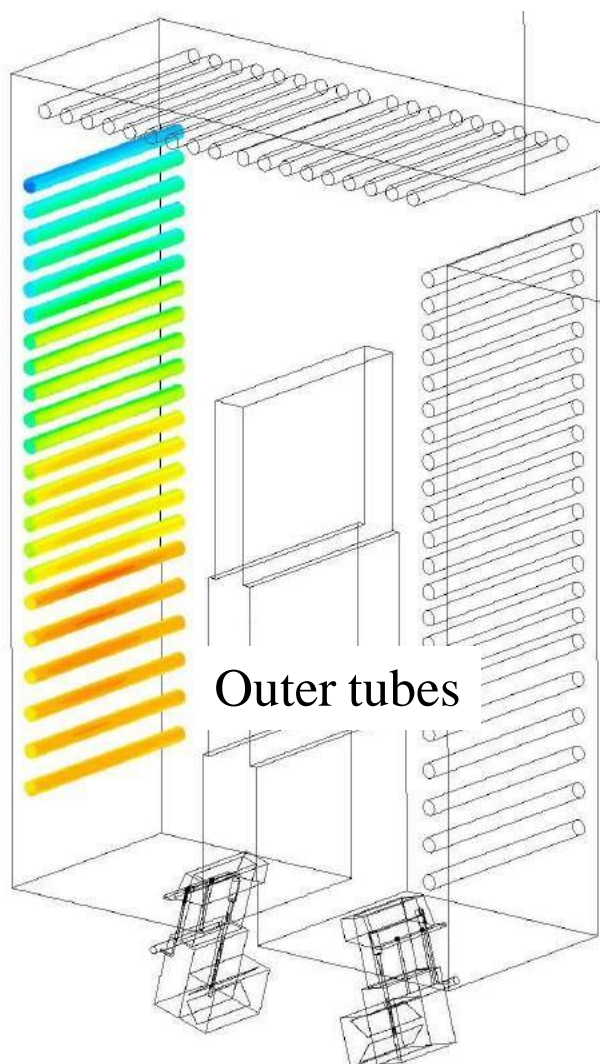
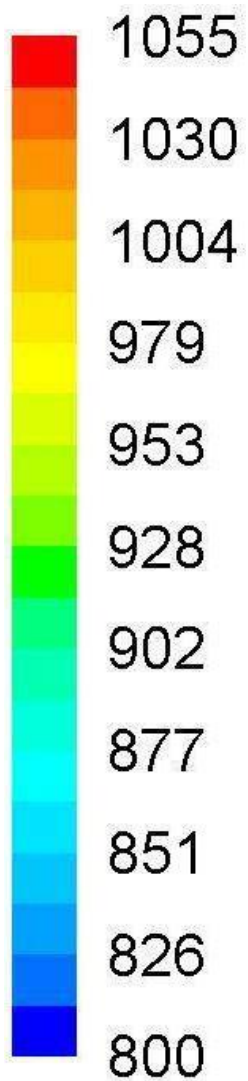
**Existing**

**Raised Tubes**

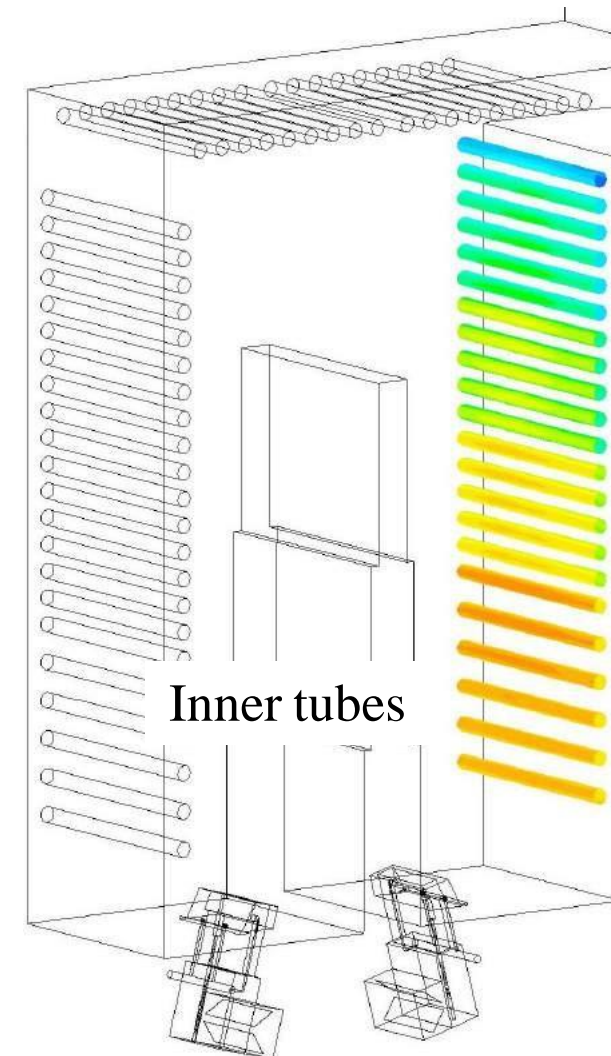


# Radiant TMT profile

[°F]



TMT profiles for inner and outer tubes are almost identical. Slight reduction in maximum TMT



**Raised Tubes**

# Proposed Design Advantages

- Radiant heat flux is reduced from 9,648 Btu/hr.ft<sup>2</sup> to 8,723 Btu/hr.ft<sup>2</sup>
- The additional area provided increase the heater capacity and enable to fire harder
- Fluid mass velocity increased from 296 lb/sec.ft<sup>2</sup> to 347 lb/sec.ft<sup>2</sup>, leading to lower coke formation
- ❖ Radiant coil pressure drop within allowable limits (350 psi)
  - Calculated pressure drop in proposed design is ~20% higher than existing



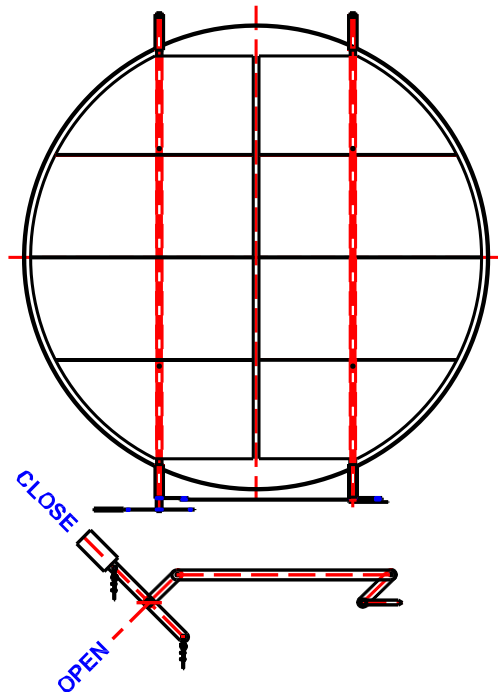
# Existing vs Proposed Operating SOR Cases

Parameters	Units	West Heater SOR Case	
		Existing	Proposed
Total Heat Duty	MMBtu/hr	94.41	94.51
Process Heat Duty	MMBtu/hr	82.83	83.18
Charge Flow Rate	lb/hr	284,683	284,683
Outlet Temperature	°F	915.2	915.2
<b>Coil Pressure Drop</b>	<b>psi</b>	<b>213.8</b>	<b>251.8</b>
Bridge Wall Temperature	°F	1,447	1,416
Radiant Heat Duty	MMBtu/hr	62.63	63.81
Radiant Heat Transfer Area	ft <sup>2</sup>	7,770	8,922
Average / Maximum Radiant Heat flux	Btu/hr/ft <sup>2</sup>	8,060 / 14,991	7,152 / 11,587
<b>Fluid Mass Velocity in Radiant Section</b>	<b>lb/sec/ft<sup>2</sup></b>	<b>320.3</b>	<b>375.2</b>
<b>Radiant Coil Pressure Drop</b>	<b>psi</b>	<b>186.4</b>	<b>226.5</b>
<b>Maximum Radiant Tube Metal Temp.</b>	<b>°F</b>	<b>966.4</b>	<b>981.6</b>

# Stack Damper Replacement

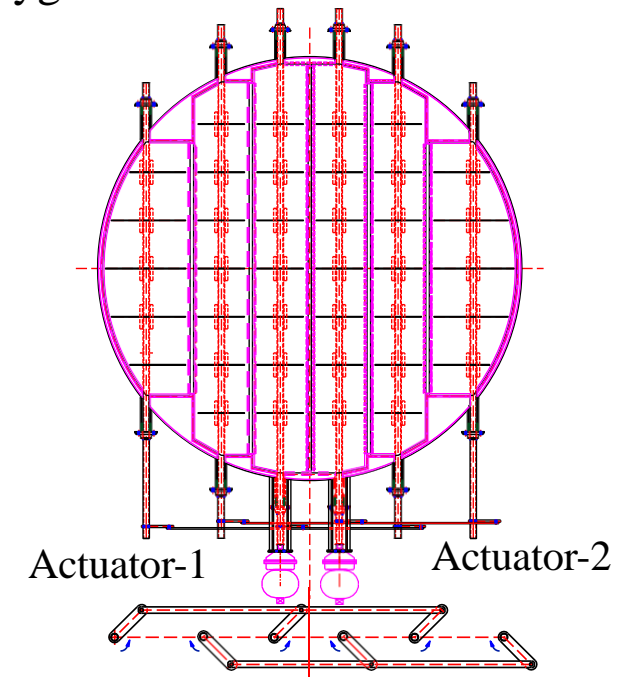
## Existing

- Stack is oversized
- Two blade Damper
- Pneumatically operated
- Heater is operating at  $\sim (-0.3)$  to  $(-0.5)$  in WC
- Unable to provide accurate draft control



## Proposed Smart Stack Damper

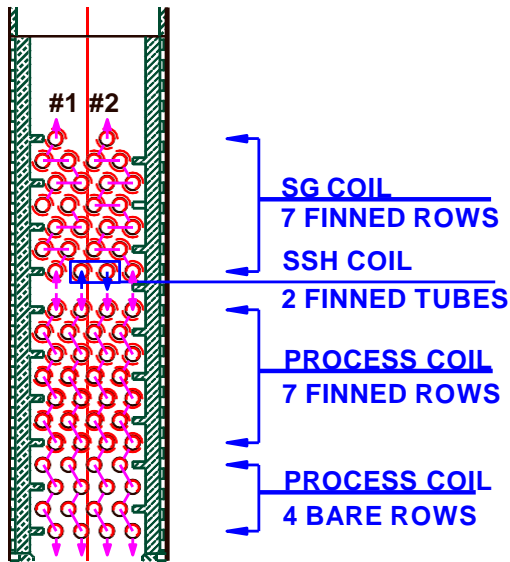
- ❖ New Damper with 6 blades and two actuators
- ❖ Two actuators link the alternate blades
- ❖ Better controlling characteristics
- ❖ Allow more pressure drop in stack
- ❖ Maintain proper draft at reduced heater loads
- ❖ Excess oxygen in firebox will be reduced



# Convection Tubes

## Existing Design

- 44 tubes with 3.5" NPS Sch 80
- Tube Pitch - 8"(H) x 8"(D)
- Tube Material – A335 Gr.P9
- Fin Details – 0.75/1" ht. x 0.06" thk x 2/3/4 FPI.

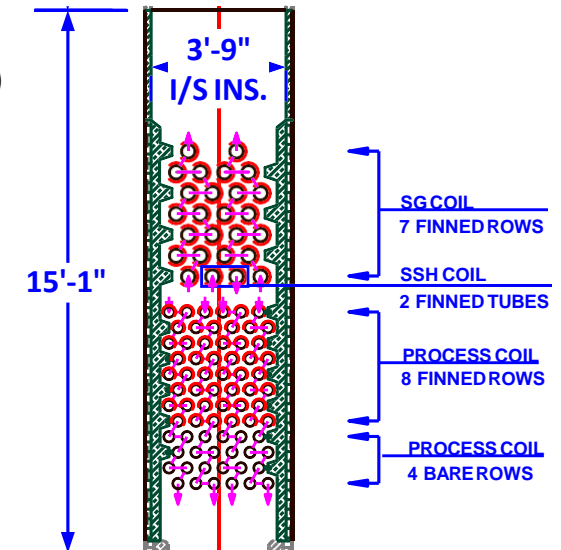


## Proposed (Not Executed)

- ❖ Increased heat transfer area, higher efficiency
- ❖ Flue gas approach temperature reduced by 170°F
- ❖ Higher fluid mass velocity of 355 lb/sec-ft<sup>2</sup> to prevent coking
- ❖ Higher fin configuration for waste heat recovery section to recover more heat

- ❖ Firing rate reduced to 135.7 MMBtu/hr

- 72 tubes with 3" NPS Sch 40
- Tube Pitch - 6"(H) x 6"(D)
- Tube Material – A335 Gr. T9
- Fin Details – 0.5/0.75" ht. x 0.06" thk x 5 FPI.



# Thank You

- We hope you will find our presentation helpful and informative
- Questions and comments are welcome